

MUSLIKH  
9008/T5  
LIGNA

**KUMPULAN GRAFIK**

**PENGANGKUTAN  
SEDIMEN**

**(SEDIMENT TRANSPORTATION)**

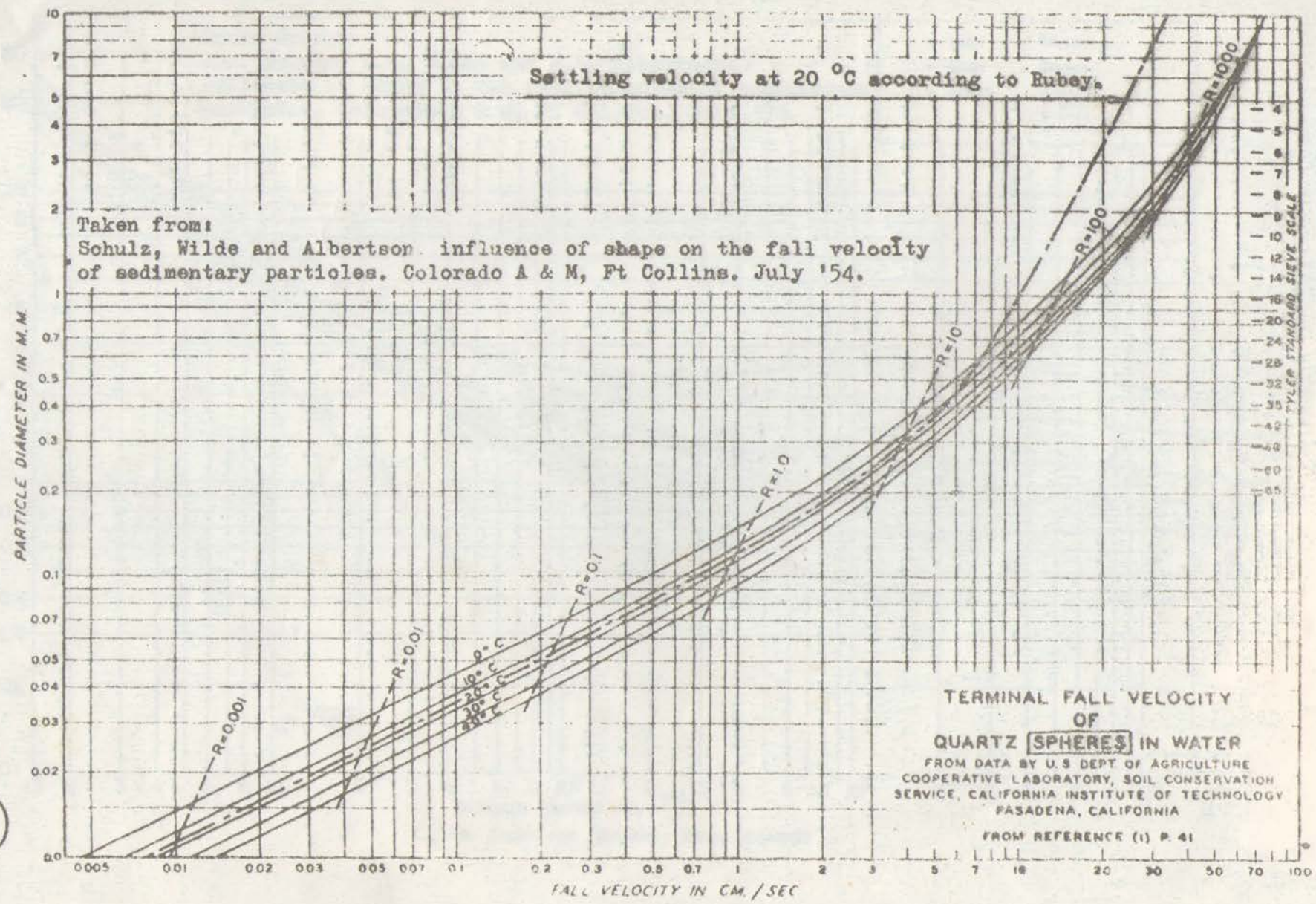


**BAGIAN TEKNIK SIPIL FAKULTAS TEKNIK U.G.M.**



Settling velocity at 20 °C according to Rubey.

Taken from:  
Schulz, Wilde and Albertson. influence of shape on the fall velocity  
of sedimentary particles. Colorado A & M, Ft Collins. July '54.



TERMINAL FALL VELOCITY  
OF  
QUARTZ SPHERES IN WATER  
FROM DATA BY U.S. DEPT. OF AGRICULTURE  
COOPERATIVE LABORATORY, SOIL CONSERVATION  
SERVICE, CALIFORNIA INSTITUTE OF TECHNOLOGY  
PASADENA, CALIFORNIA  
FROM REFERENCE (1) P. 41

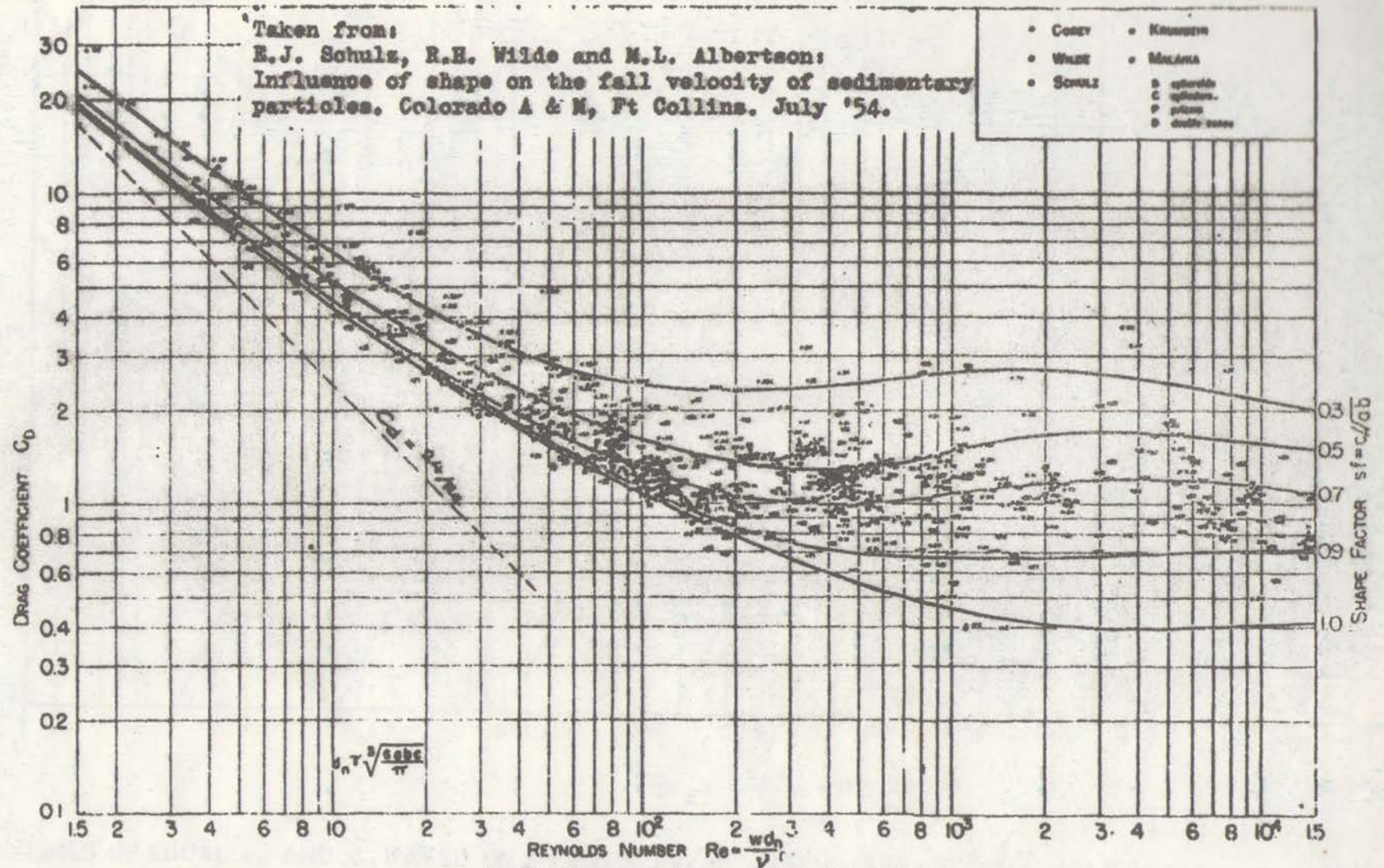
TS

MUSLIKHT  
S008/TS  
U5M



Taken from:  
 E.J. Schulz, R.H. Wilde and M.L. Albertson:  
 Influence of shape on the fall velocity of sedimentary  
 particles. Colorado A & M, Ft Collins. July '54.

- COLEY
- WILST
- SCHULZ
- KRAMER
- MACANA
- spheroids
- cylinders
- △ prisms
- ◇ double cones



$$v_n = \sqrt{\frac{8cgs}{\pi}}$$

$C_D \cdot Re$  GRAPH FOR NATURALLY WORN SEDIMENTS

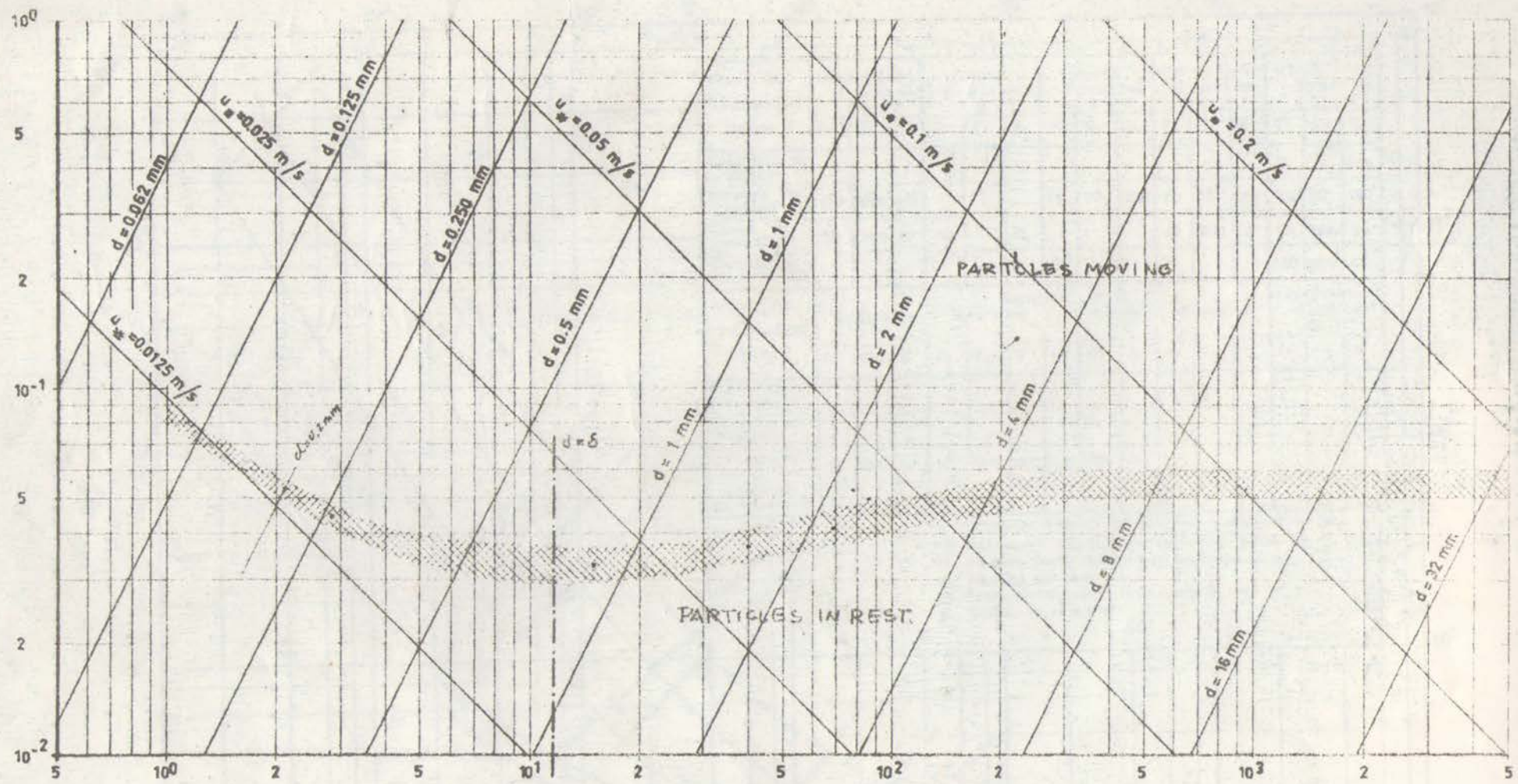
52



$$\left[ \frac{u_*^2}{\frac{\rho_s - \rho_w}{\rho_w} g d} \right]$$

OR

$$\frac{\tau_c}{(\rho_s - \rho_w) g d}$$

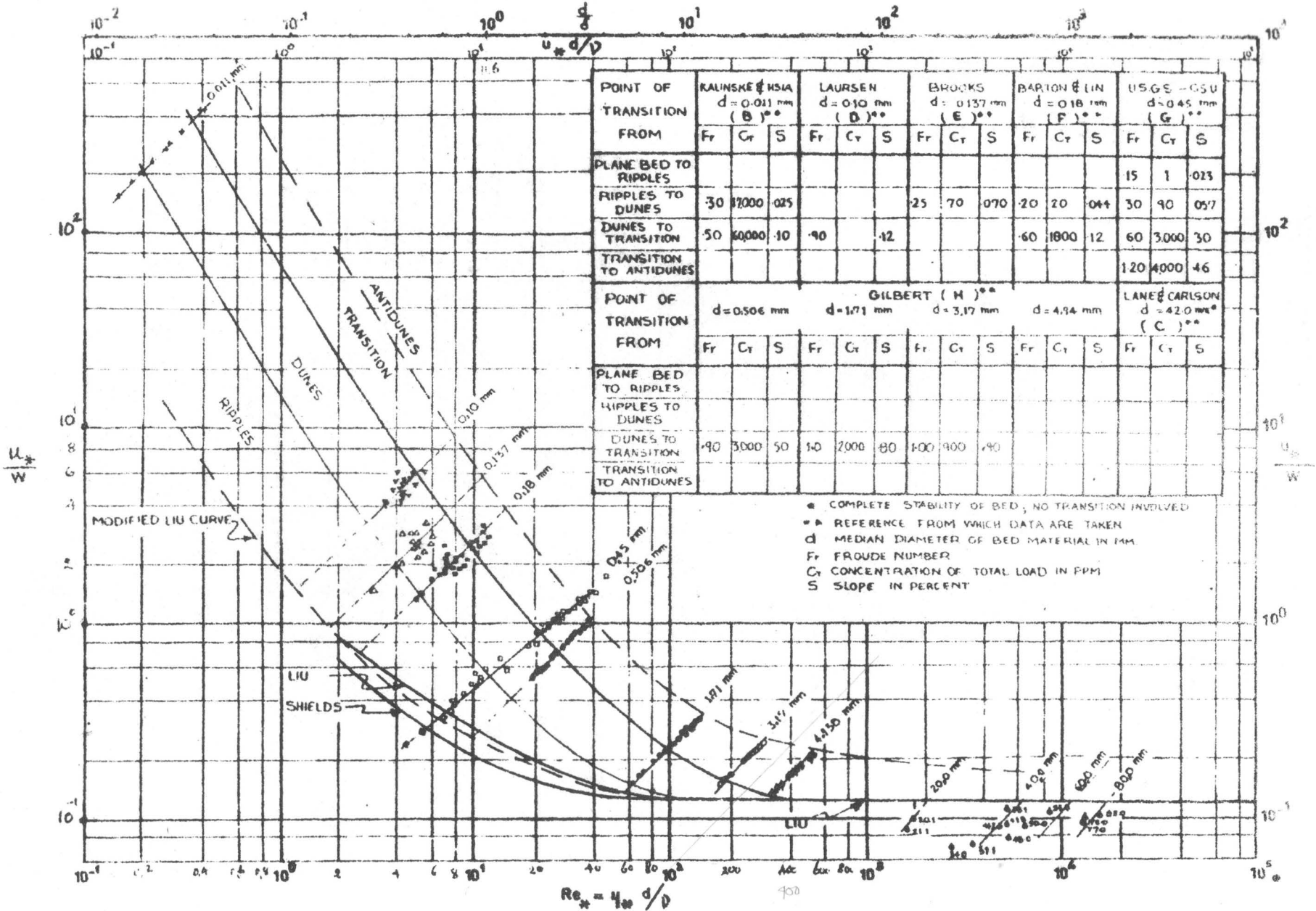


(S)

$$Re_* = \frac{u_* d}{\nu} = 11.6 \frac{d}{\delta}$$

LINES OF EQUAL  $u_*$  AND  $d$  BASED ON  $\rho_s = 2650 \text{ kg/m}^3$  AND  $\nu = 1.25 \times 10^{-6} \text{ m}^2/\text{s}$  (12 °C)

RELATIONSHIP OF CRITICAL SHEAR STRESS AND DIAMETER FOR A BED OF UNIFORM GRAINS. ACC. TO SHIELDS (1936)



CRITERIA FOR ROUGHNESS IN ALLUVIAL CHANNELS

FROM ALBERTSON ET AL (1958)  
ASCE PAPER 1558 PG 23

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DISTRIBUTION OF TRACTIVE FORCE IN CHANNELS  
 (Illustration taken from table 5, Lane 1955)

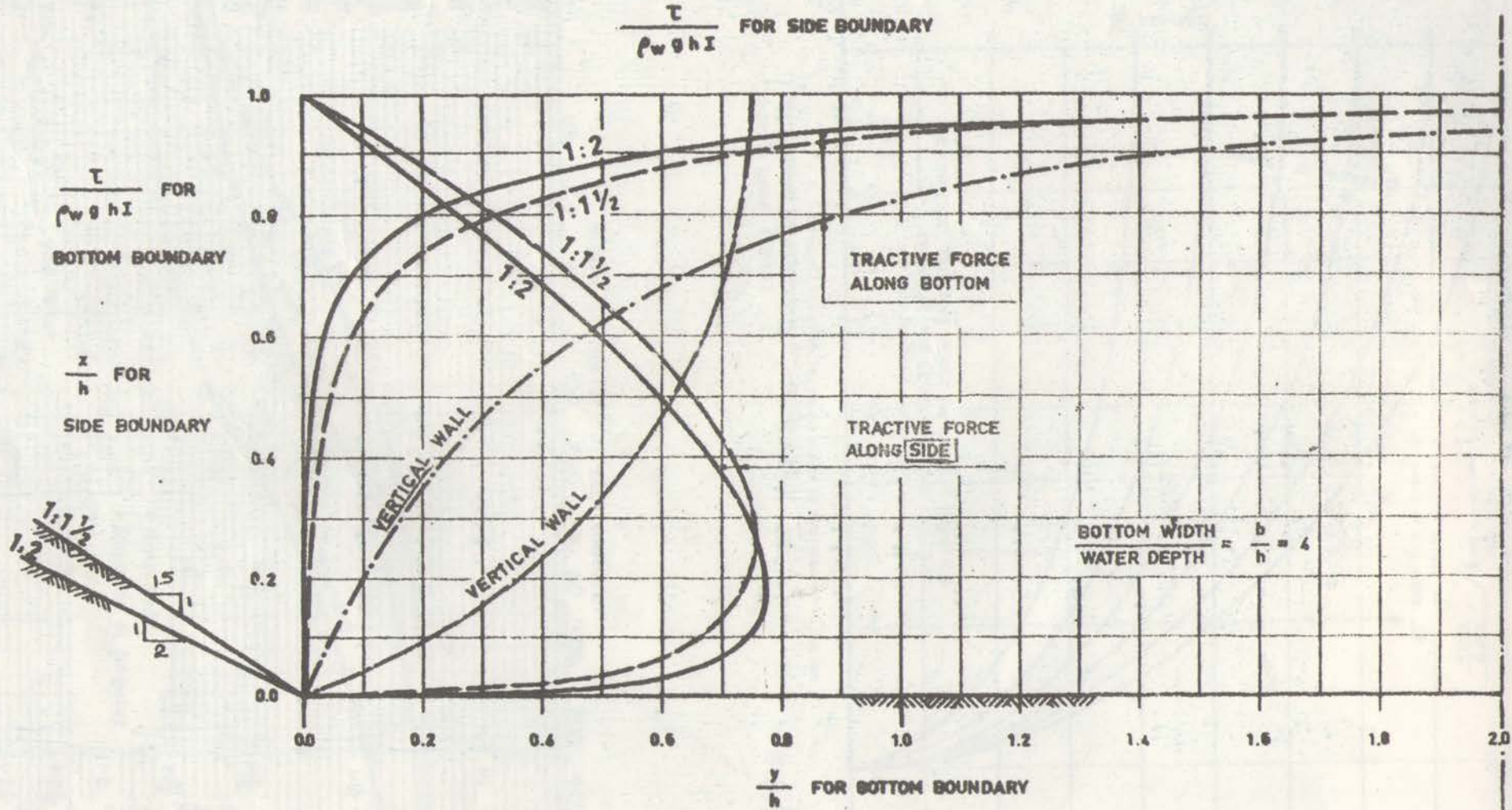


FIG. A  
 55







Acc. to EINSTEIN (1950)

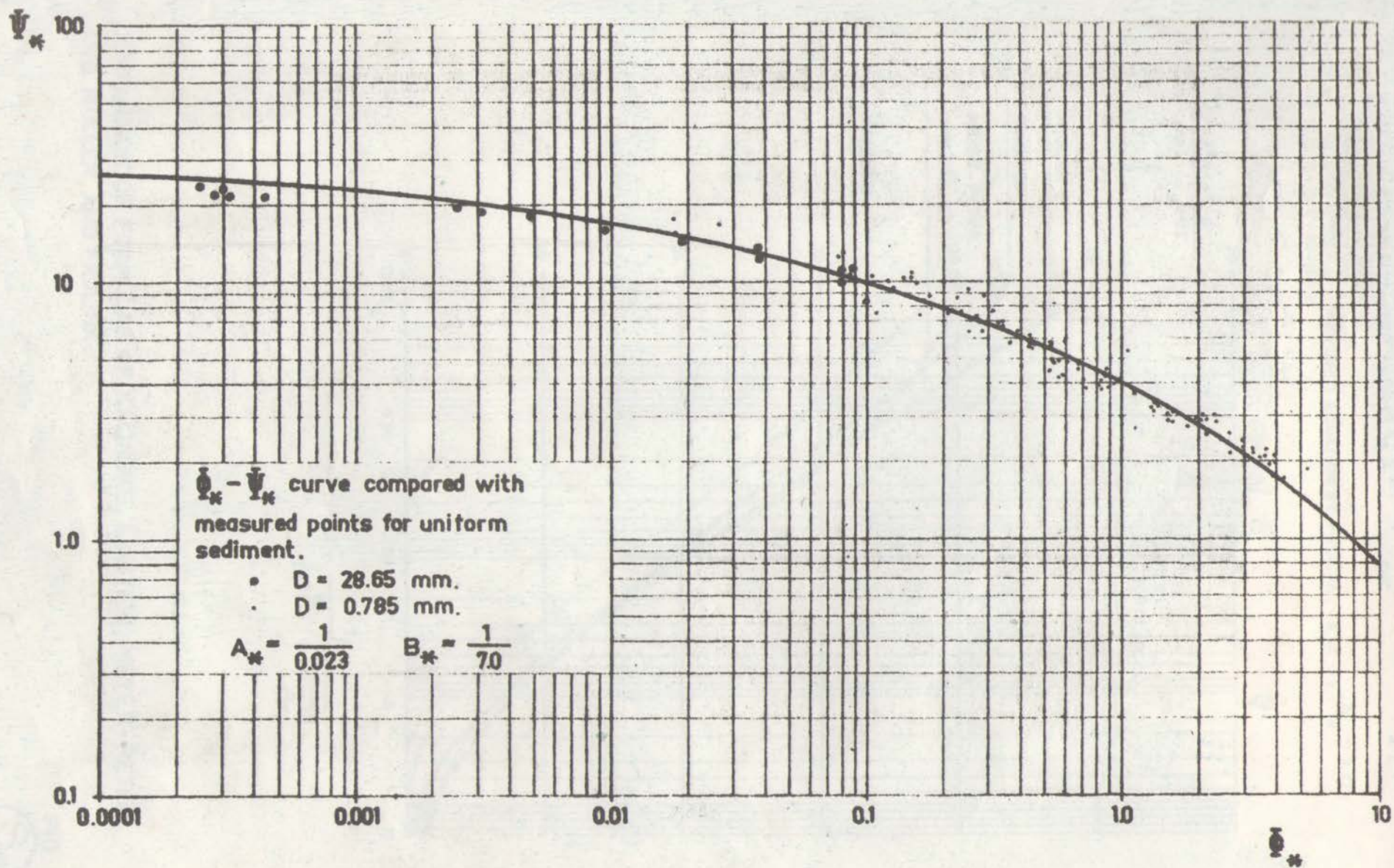
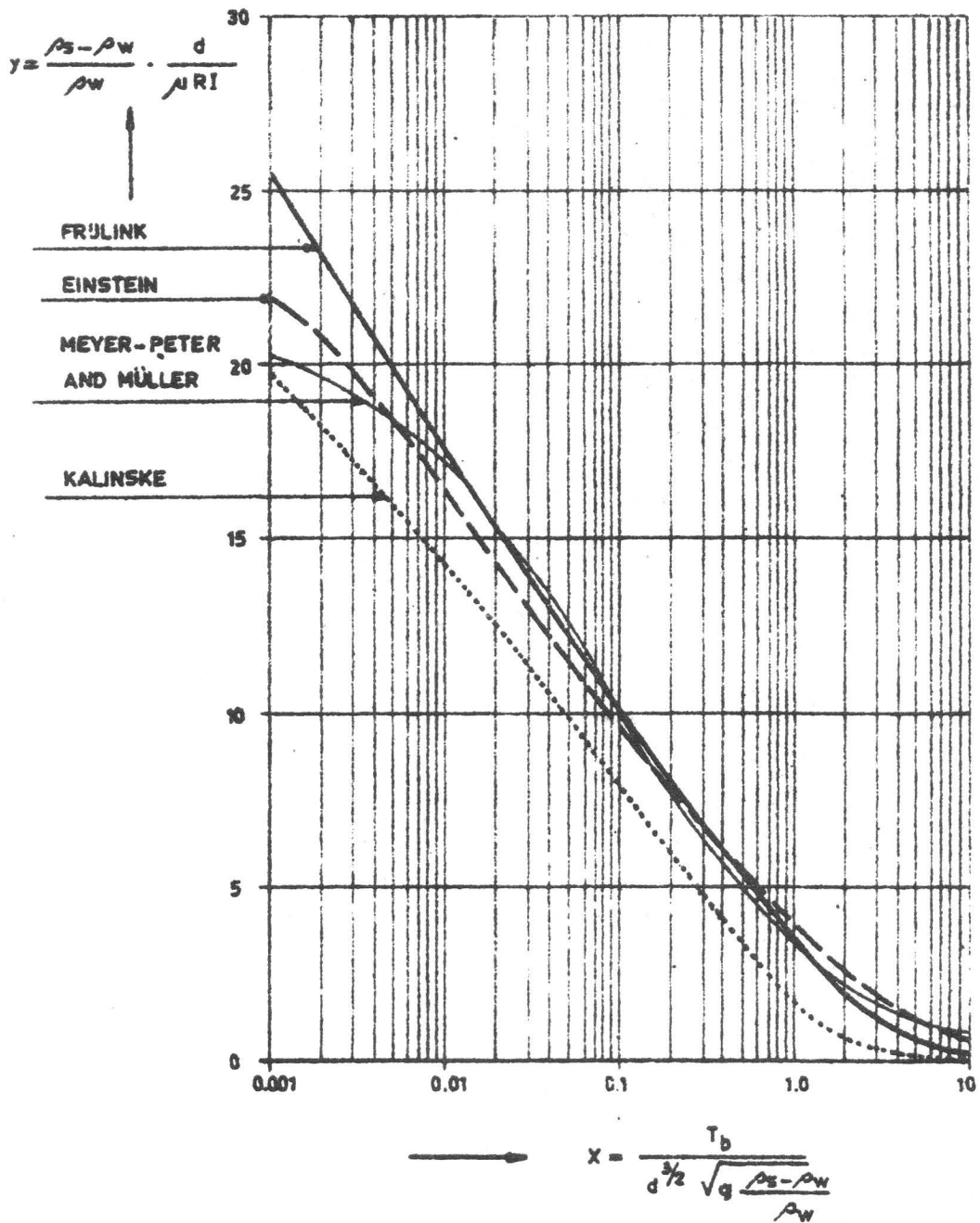


FIG. E  
S7



PROPOSED EQUATION BY FRULINK:  $x = 5y^{-\frac{1}{2}} e^{-0.27y}$



COMPARISON OF FORMULAE OF KALINSKE, EINSTEIN, MEYER-PETER AND MULLER, AND FRULINK.



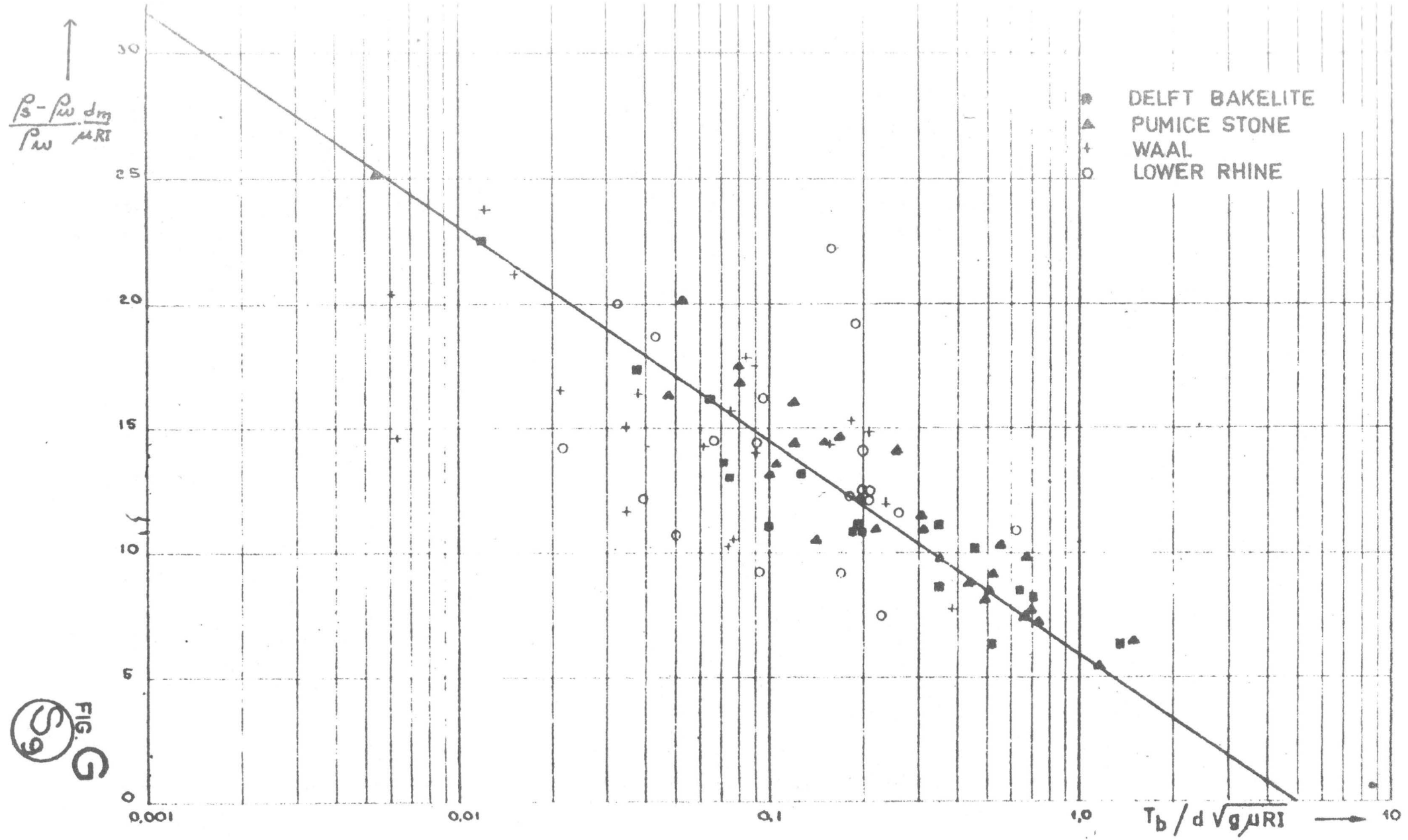
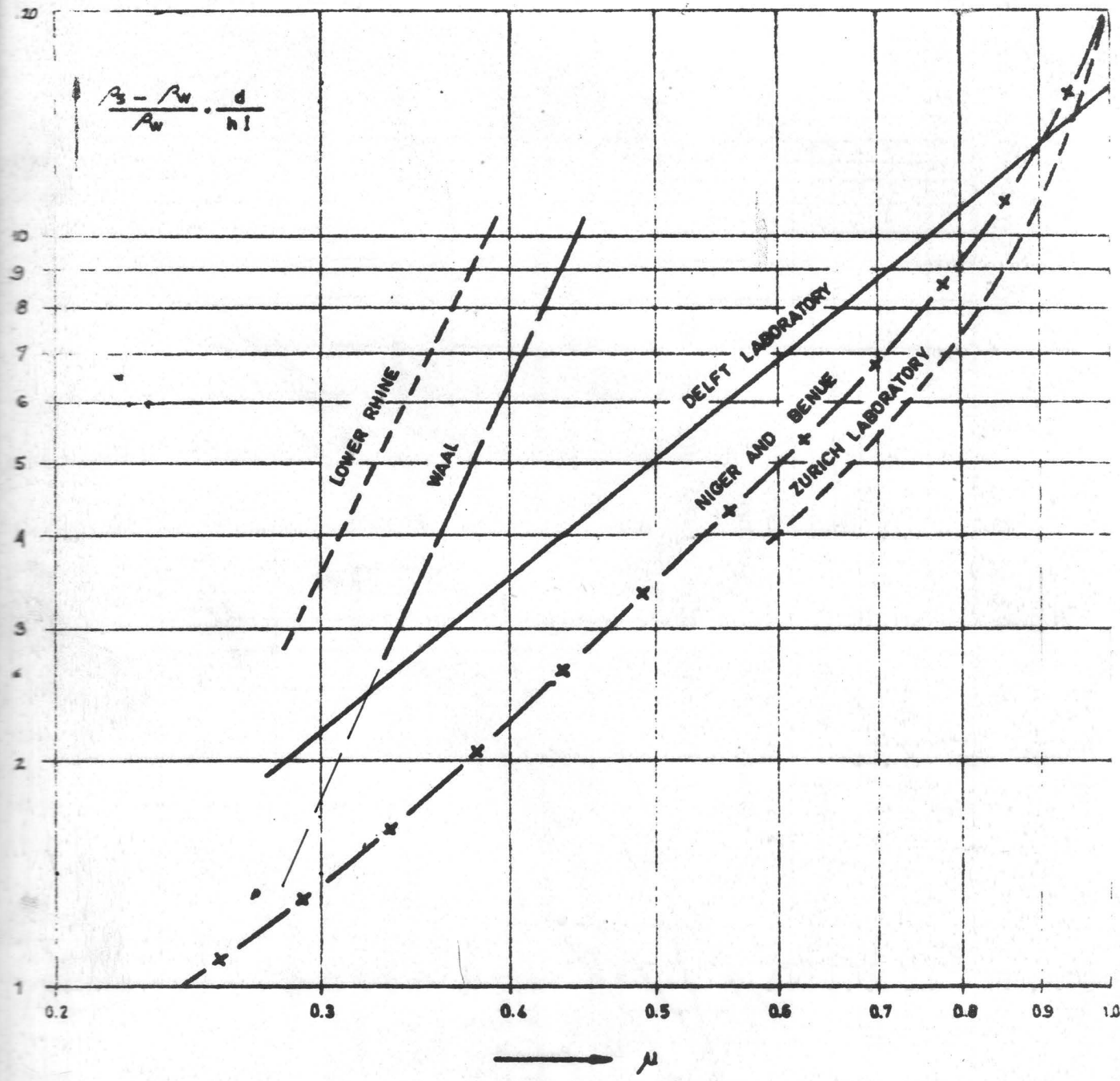


FIG 5  
 (59)

SIMPLIFIED BED-LOAD EQUATION ACC. TO FRJLINK (1952)  
 MODEL-AND PROTOTYPE MEASUREMENTS





EXPERIMENTAL RELATIONSHIPS BETWEEN RIPPLE-FACTOR  $\mu$

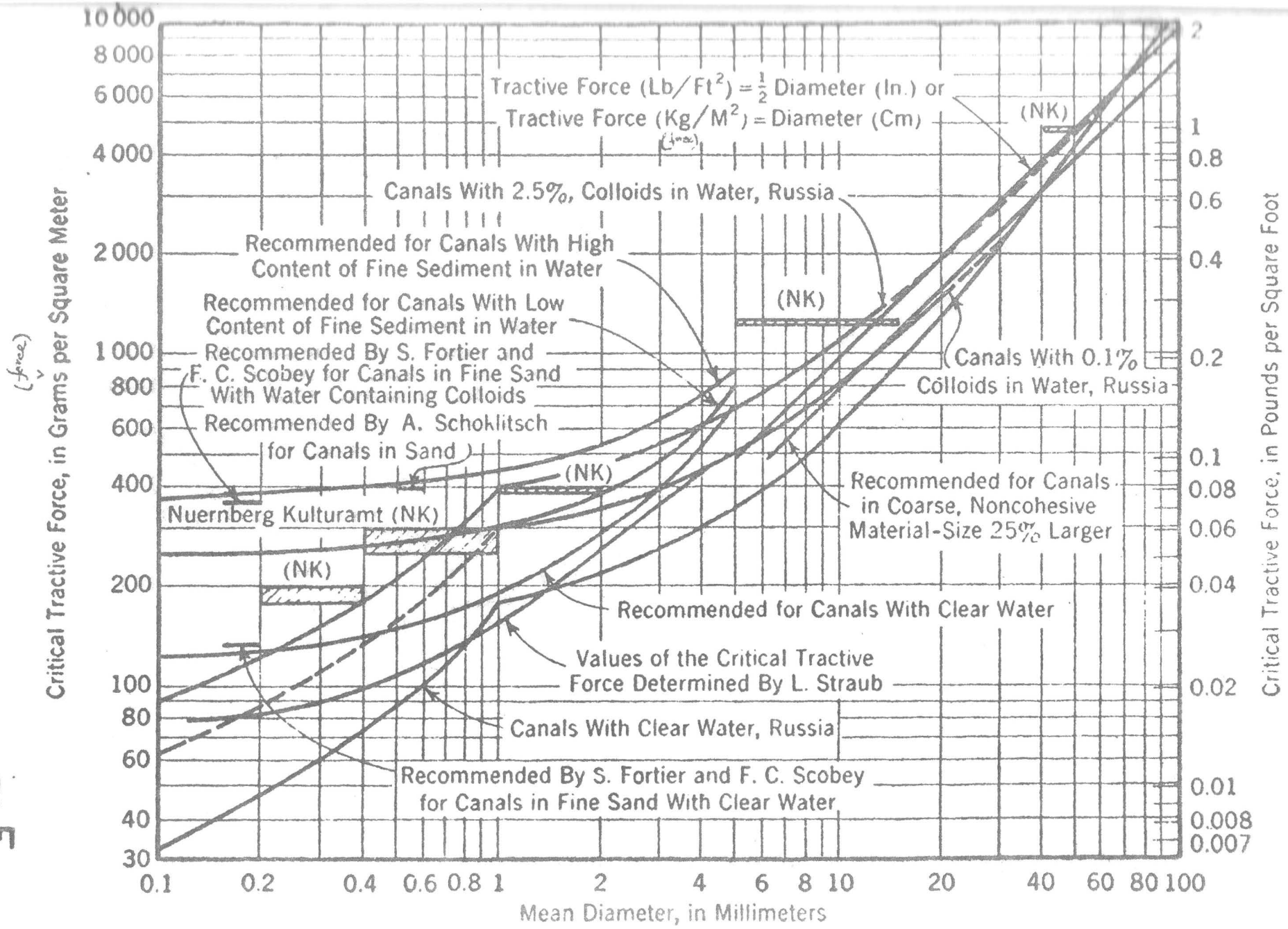
AND  $\frac{\rho_s - \rho_w}{\rho_w} \cdot \frac{d}{hl}$

Acc. to Frijlink (1952)



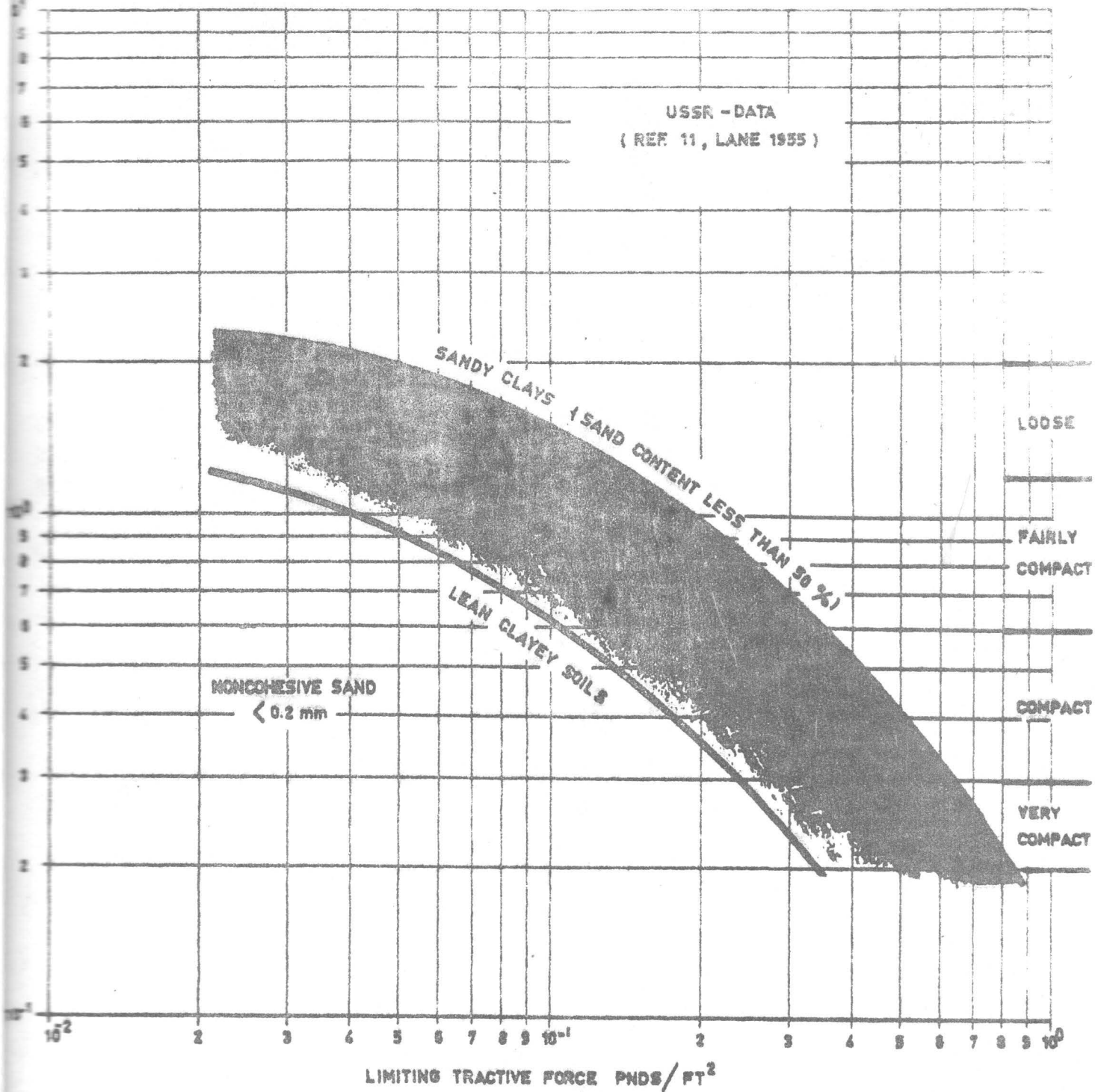


FIG. F  
S 11



RECOMMENDED LIMITING TRACTIVE FORCES FOR CANALS  
Acc to Long (1955)

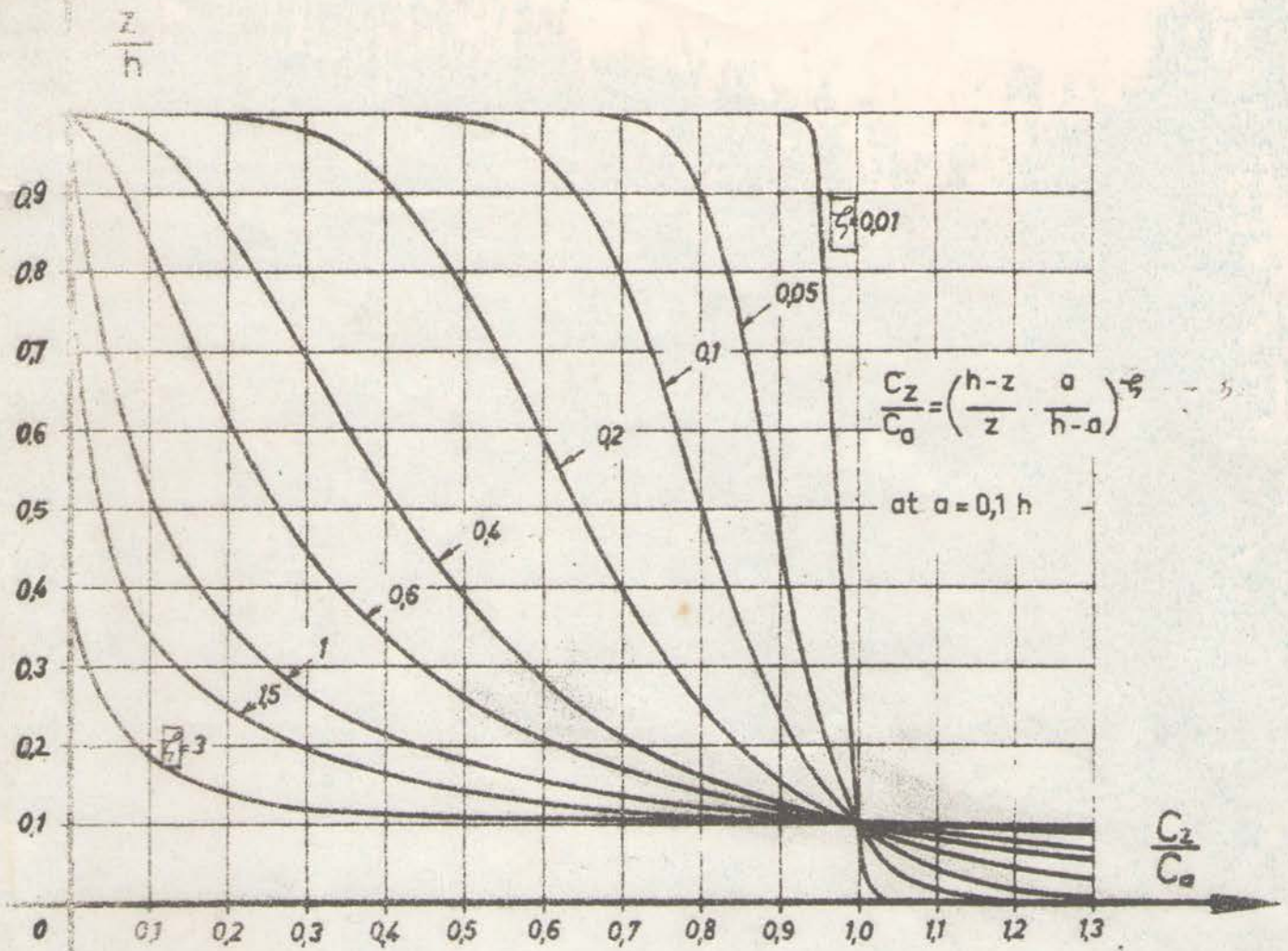
$$\text{EM RATIO} = \frac{\text{Vol. of voids}}{\text{Vol. of solids}} \times 100\%$$



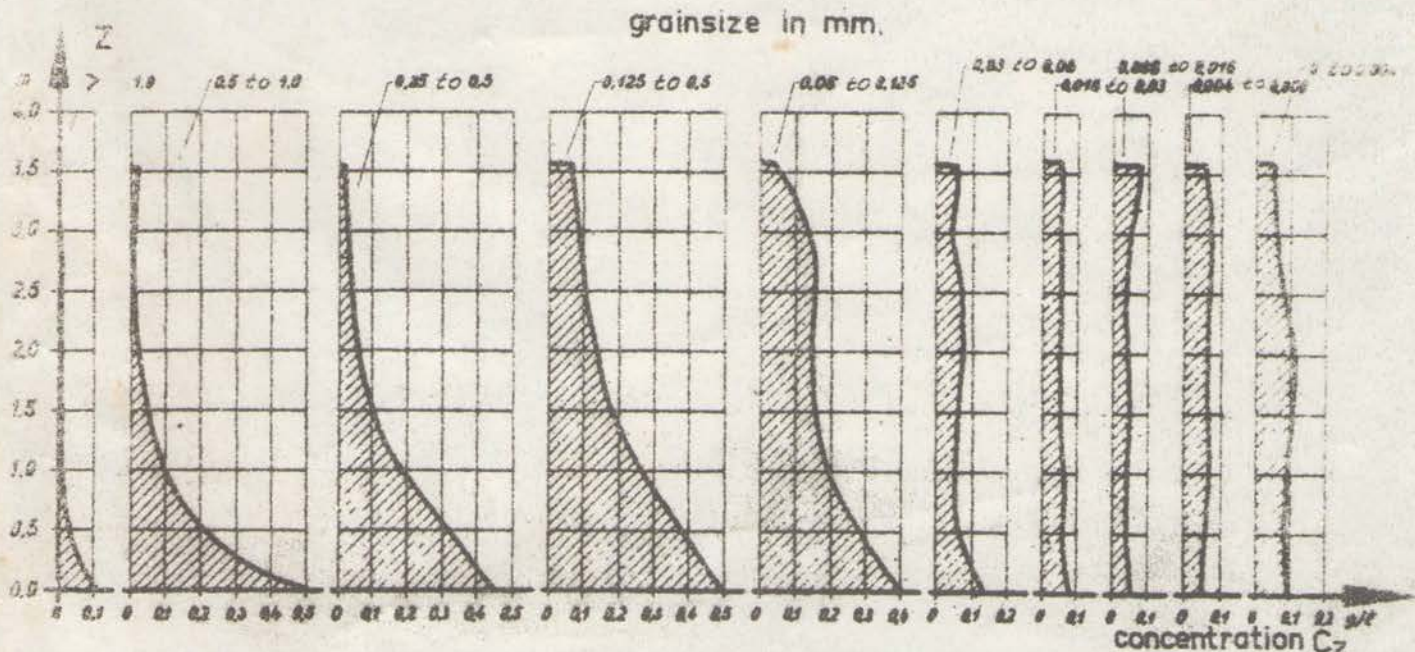
TRACTION FORCES IN COHESIVE MATERIAL.

FIG. G  
S<sub>12</sub>





DISTRIBUTION OF SUSPENSION AS A FUNCTION OF  $\xi$



DISTRIBUTION OF SUSPENSION IN THE MISSOURI RIVER.

S<sub>13</sub>

FIG. A